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# HIGH-LATITUDE PHOTODISSOCIATION RATES AND PREDICTED SOLAR FLUX INTENSITIES

An Addendum to ECOM-77-1, "STRATCOM-Related  
Photodissociation Rates and Solar Flux Intensities"

By

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US Army Electronics Command

White Sands Missile Range, New Mexico 88002

**July 1977**

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Photodissociation rates and predicted solar flux intensities have been reported previously by J. L. Collins for conditions closely corresponding to those of the STRATCOM (STRATospheric COMposition) balloon launches made by the Atmospheric Sciences Laboratory (ASL) at Holloman Air Force Base, New Mexico. This brief addendum to that report extends the calculations to include rates and solar flux intensities predicted for 65.3° north latitude. This is the location of the U. S. Army's Meteorological Rocket Station at Poker Flat, Alaska, where it is possible that such correlated experiments as the STRATCOM balloon launches			

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20. ABSTRACT (cont)

will be made in the future.

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## 1. INTRODUCTION

Photodissociation rates have been reported recently<sup>1</sup> for 32° north latitude. These values were calculated for conditions closely corresponding to those of the STRATCOM balloon launches made by ASL at Holloman Air Force Base, New Mexico, as part of their experimental program to study the structure and composition of the upper atmosphere.

Future measurements could include balloon launches made from experimental stations at other latitudes; therefore, this brief addendum to the original report includes twenty-four photodissociation rates calculated for thirteen atmospheric species in the 10-50 altitude interval for 65.3° north latitude, the location of the U. S. Army's Meteorological Rocket Station in Poker Flat, Alaska. For purposes of comparison, these calculations were made for September 25, the date of calculations made for 32° north latitude.

## 2. INPUT DATA AND COMPUTATIONAL METHOD

Initially, photodissociation rates were calculated using the standard 32° north density profiles except for ozone and nitric acid. The ozone profile is based on the February-March 1975 measurements of Randhawa<sup>2</sup> at Poker Flat, with his best estimate for the seasonal variation and nitric acid being arbitrarily increased by about 30 percent. These initial rates were used in the ASL Chemical Kinetic Model, ASA<sup>3</sup>, to predict new profiles using Olsen's<sup>4</sup> experimental temperature profile taken at Poker Flat during February-March 1975 with adjusted O<sub>2</sub> and N<sub>2</sub> profiles from the Fort Creely<sup>5</sup> model atmosphere (64° north latitude). The input density profiles for H<sub>2</sub>O, NO<sub>2</sub>, NO, N<sub>2</sub>O, HNO<sub>3</sub>, CO<sub>2</sub> and CH<sub>4</sub><sup>6-22</sup> were adjusted based on recent measurements, most of which were made at higher latitudes.

Using the profiles predicted by ASA, the photodissociation rates and solar flux intensities were recalculated, and a second calculation of the profiles was made using the new rates.

### 3. RESULTS

The numerical values of photodissociation reaction rates calculated for the maximum solar zenith angle on September 28, 1976, at 65.3° north latitude are listed with those previously reported for 32° north latitude for the convenience of the user. These values may be found in Appendix A with computerized plots of the high latitude rates. As before, zero rates are tabulated as  $1.0 \times 10^{-24}$ .

Plots of the solar flux at typical balloon flight altitudes are given in Figures 3.1 through 3.5.



FIG. 3.1 SOLAR FLUX INTENSITIES PREDICTED AT 47.5 KM.

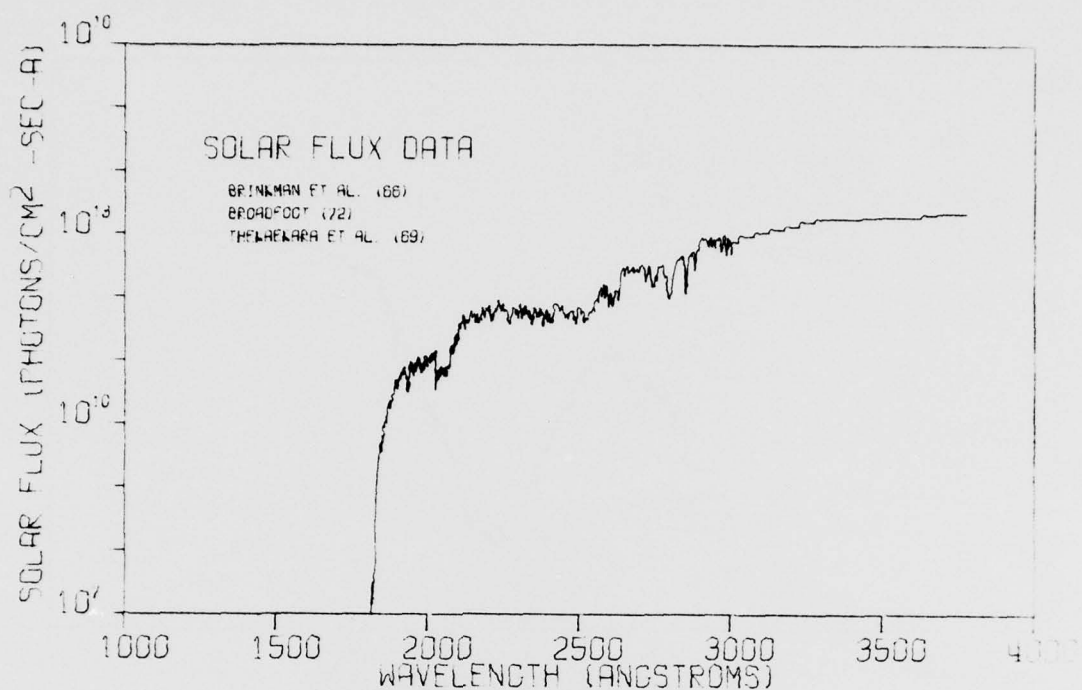


FIG. 3.2 SOLAR FLUX INTENSITIES PREDICTED AT 42.5 KM.

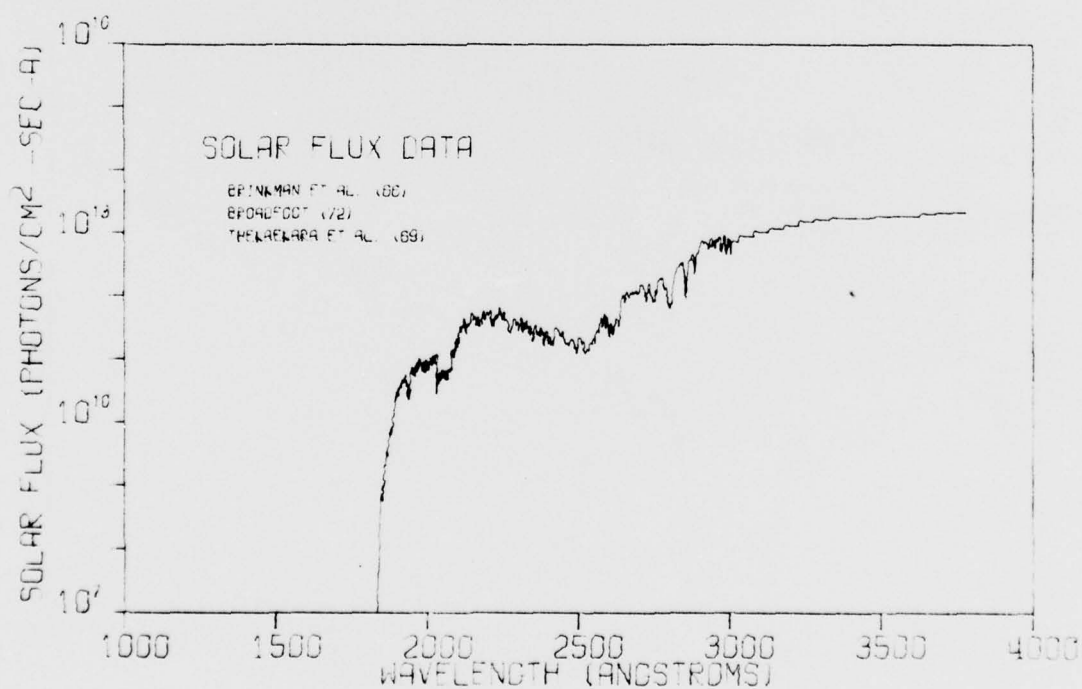


FIG. 3.3 SOLAR FLUX INTENSITIES PREDICTED AT 37.5 KM.

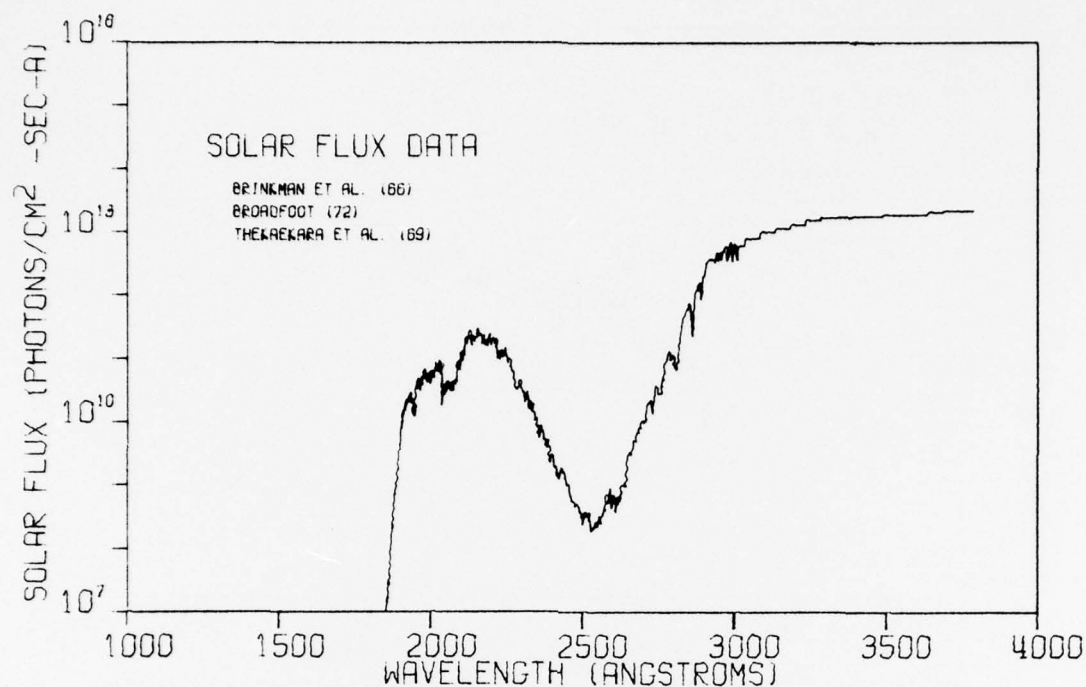


FIG. 3.4 SOLAR FLUX INTENSITIES PREDICTED AT 32.5 KM.

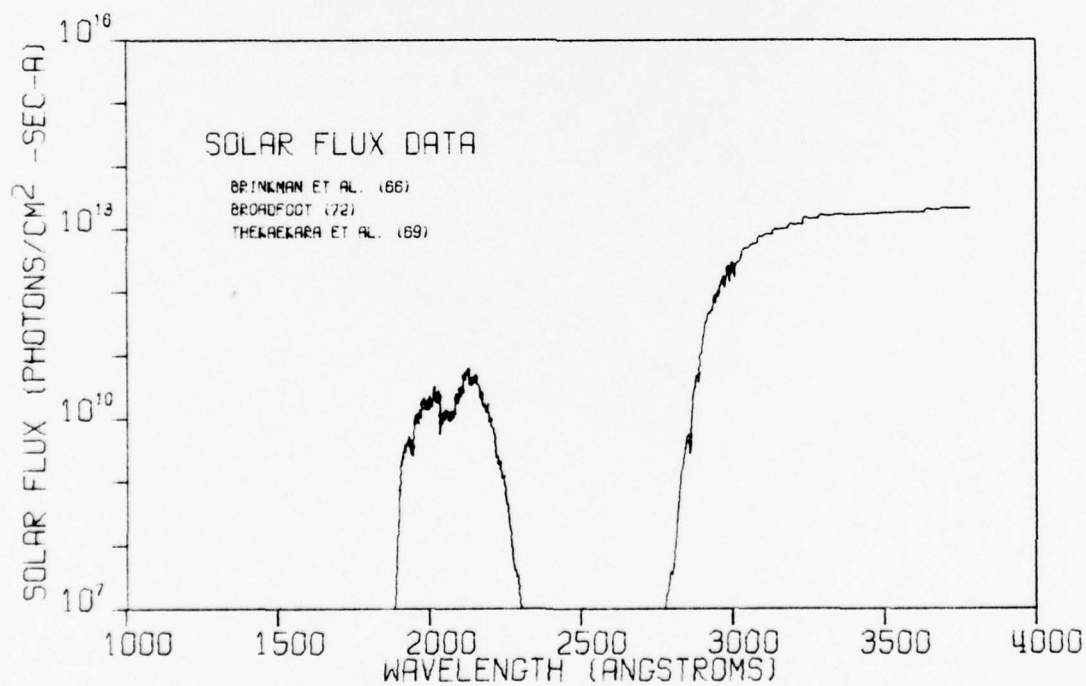
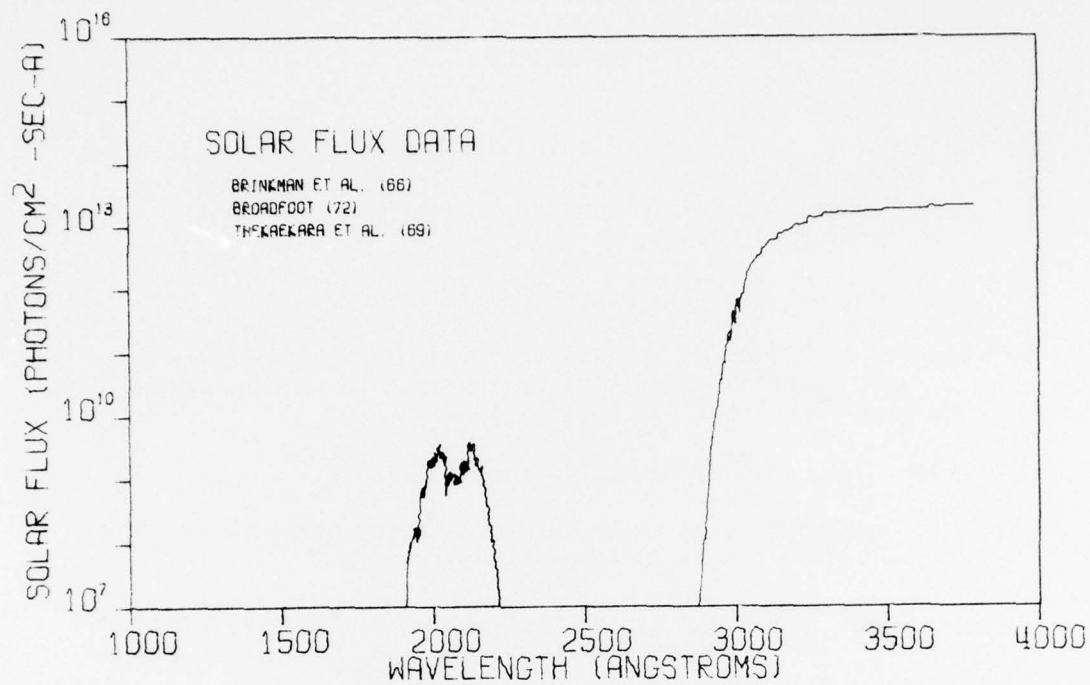


FIG. 3.5 SOLAR FLUX INTENSITIES PREDICTED AT 27.5 KM.



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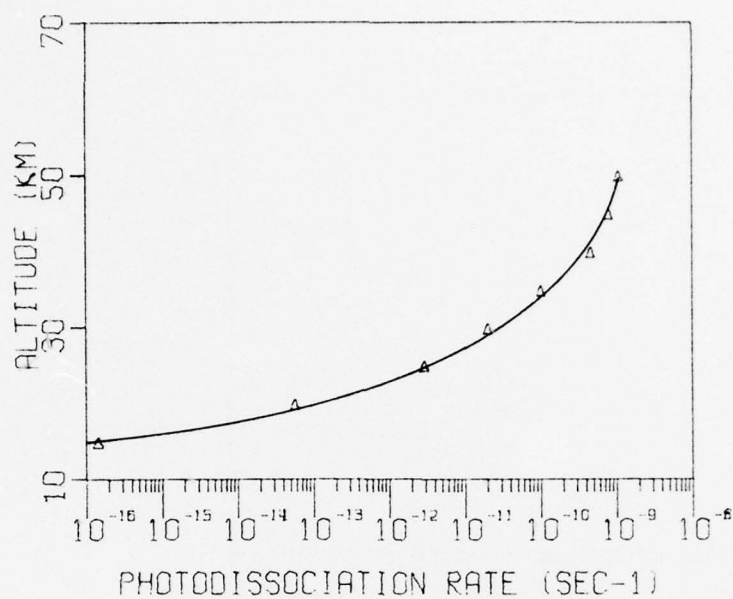
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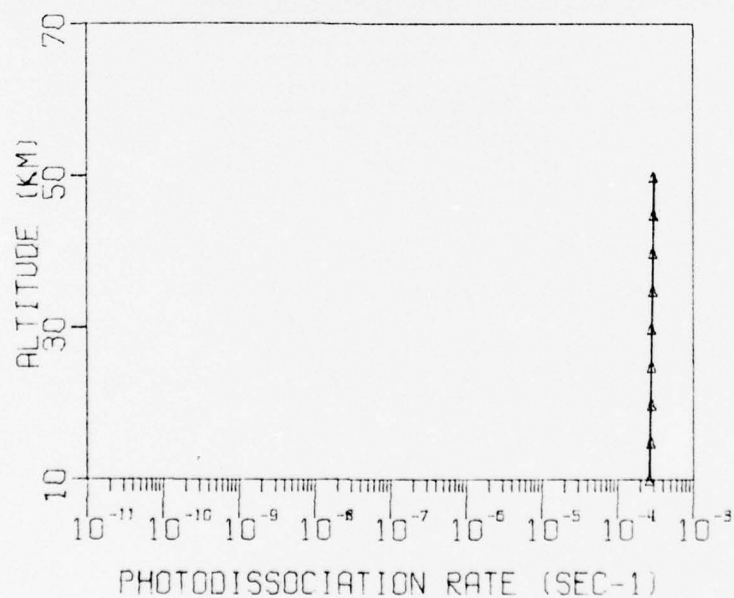
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# APPENDIX A

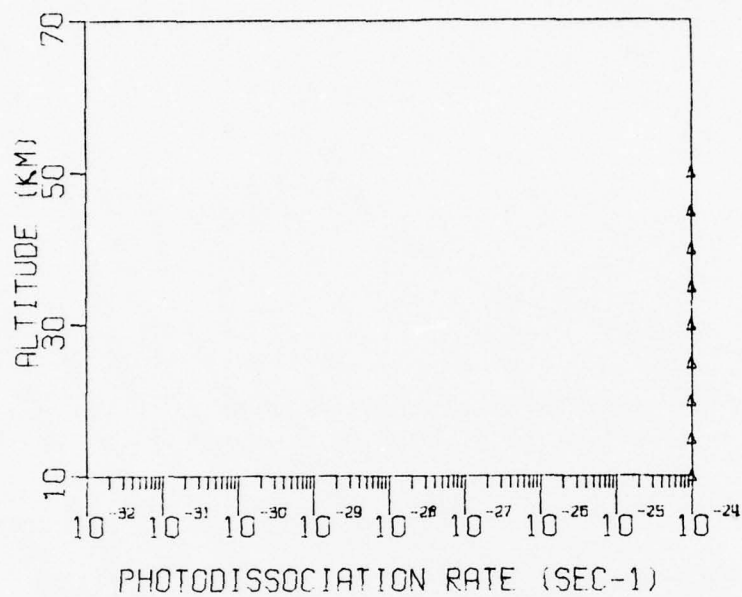
## PHOTODISSOCIATION RATES



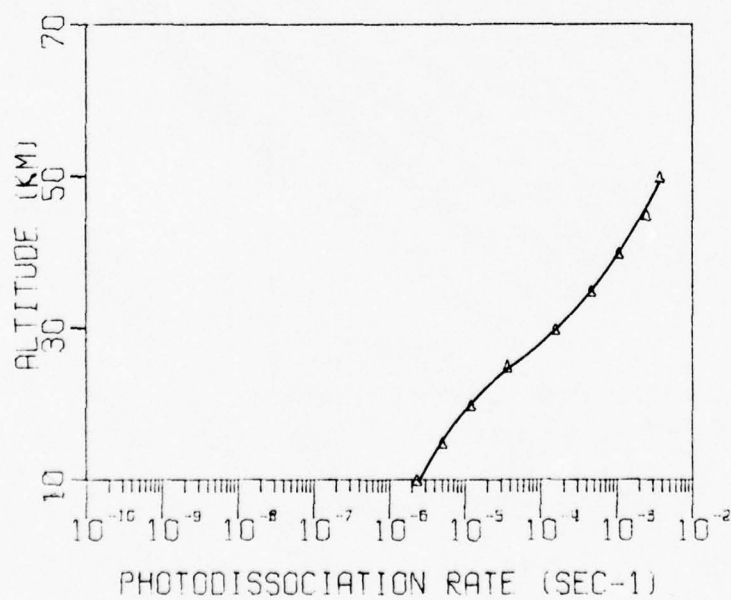
1  $O_2 + h\nu = O + O$  175.9-242.4 NM.  $\phi = 1.000$



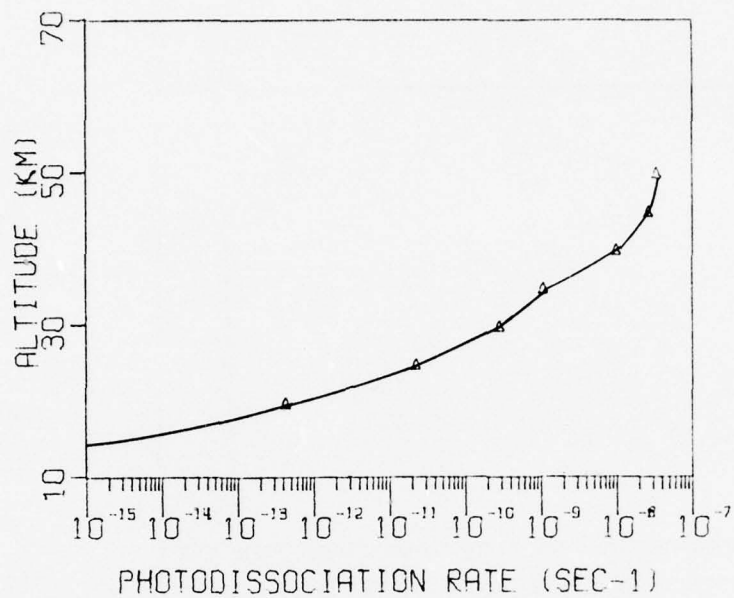
5  $O_3 + h\nu = O + O_2$  [440.0]  $\phi = 1.000$



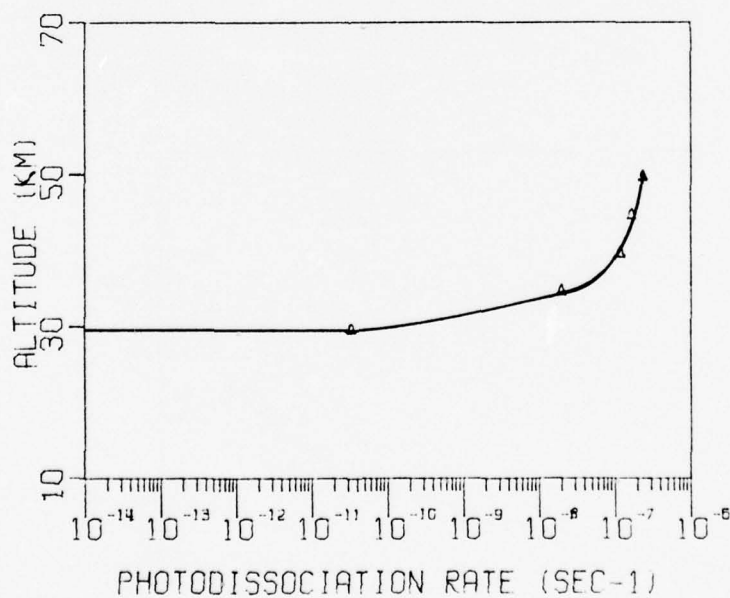
6  $O_3 + h\nu = O + O_2(1D)$  310.0-360.0 NM.



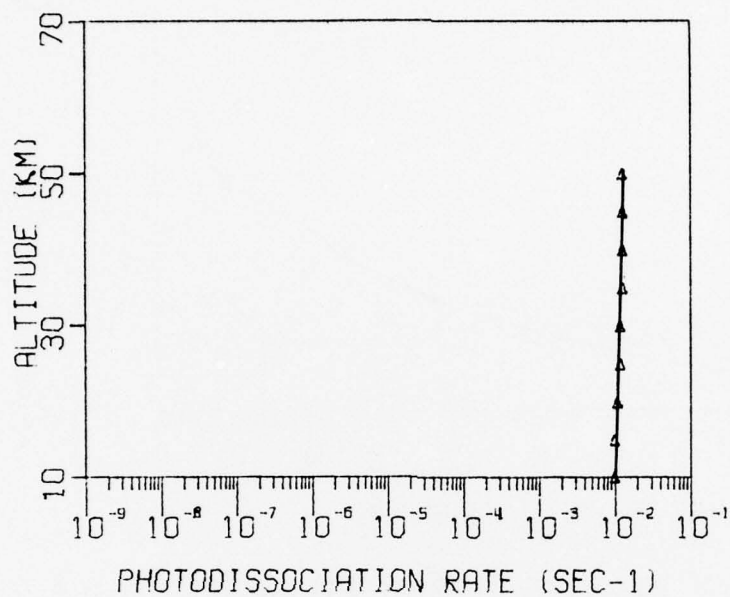
7  $O_3 + h\nu = O(1D) + O_2(1D)$  [310.0 NM.]  $\lambda$  IS VARIABLE



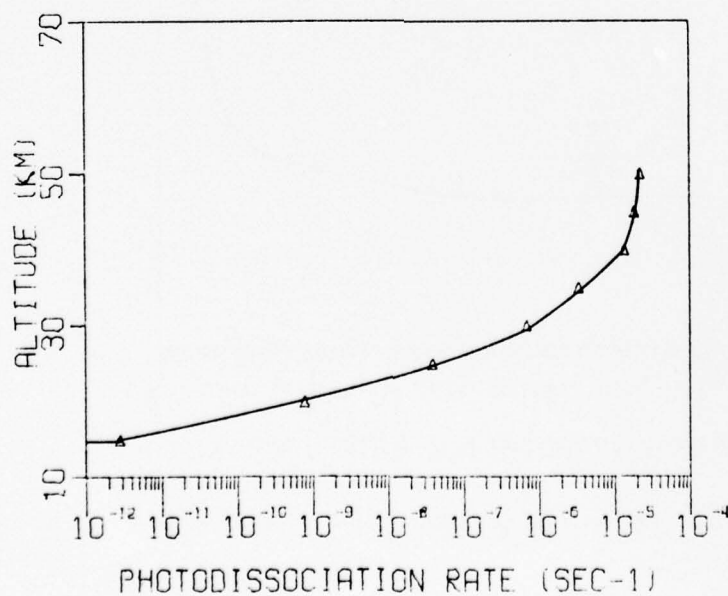
8  $O_3 + h\nu = O1S + O21D$  [199.0 NM.]  $\phi = 0.01$



9  $O_3 + h\nu = O + O21S$  [266.0 NM.]  $\phi = 0.05$

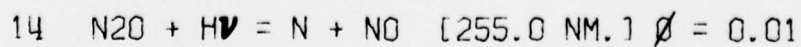
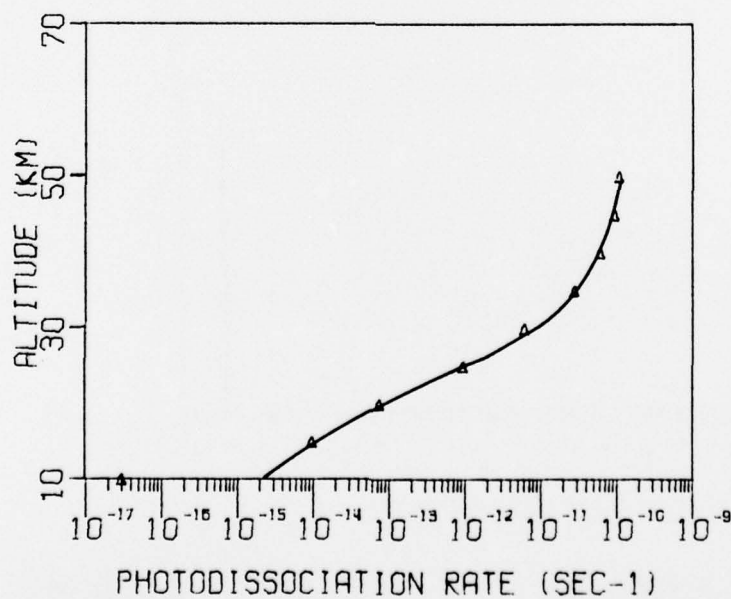
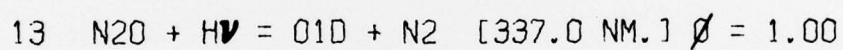
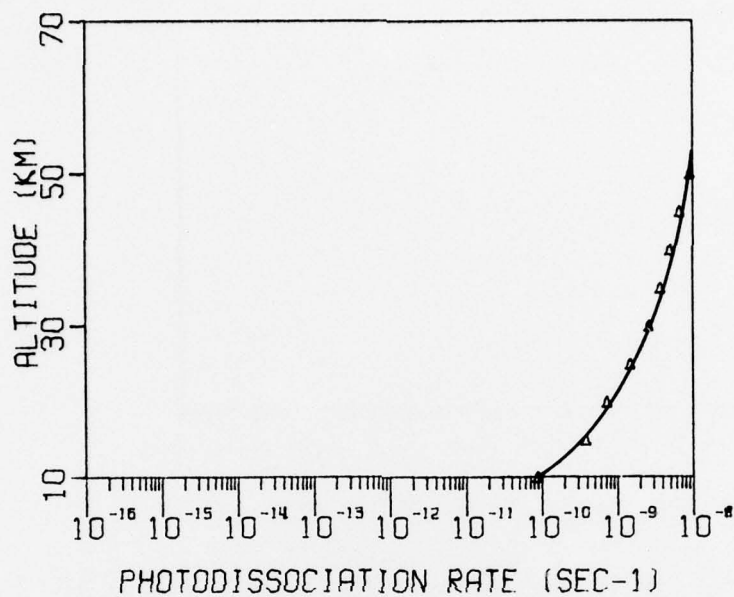


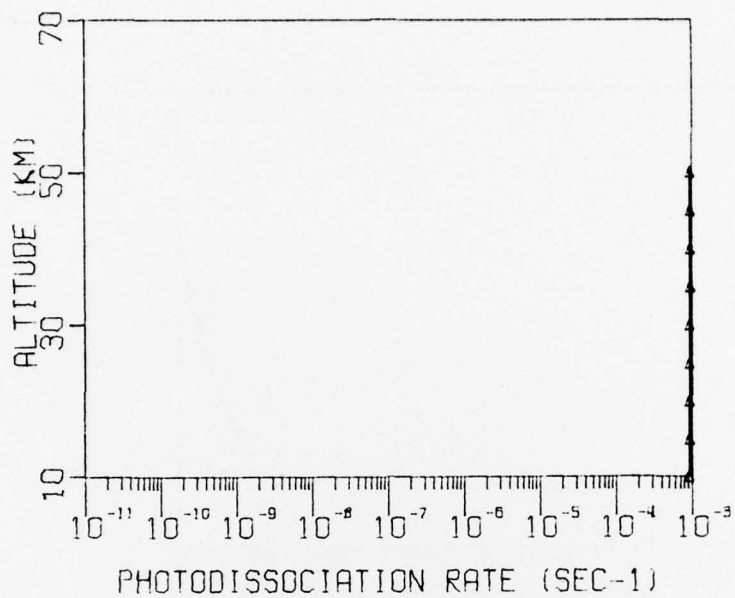
11  $\text{NO}_2 + \text{h}\nu = \text{O} + \text{NO}$  ( $\lambda > 190.01$  nm)  $\phi$  IS VARIABLE



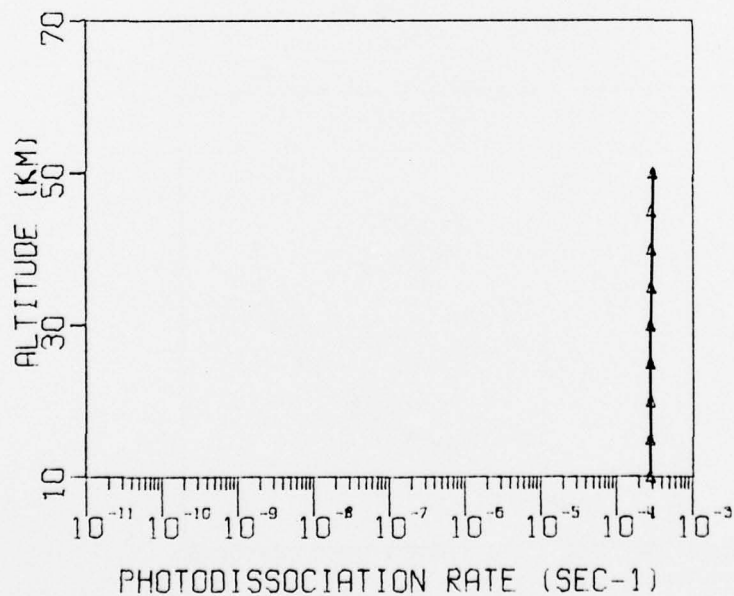
12  $\text{NO}_2 + \text{h}\nu = \text{O}(1\text{D}) + \text{NO}$  ( $\lambda < 190.01$  nm)  $\phi = 0.02-0.05$



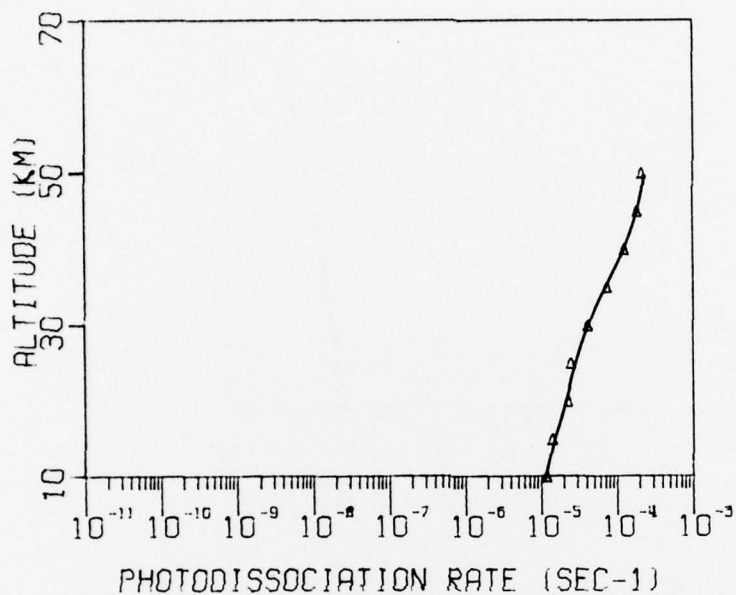




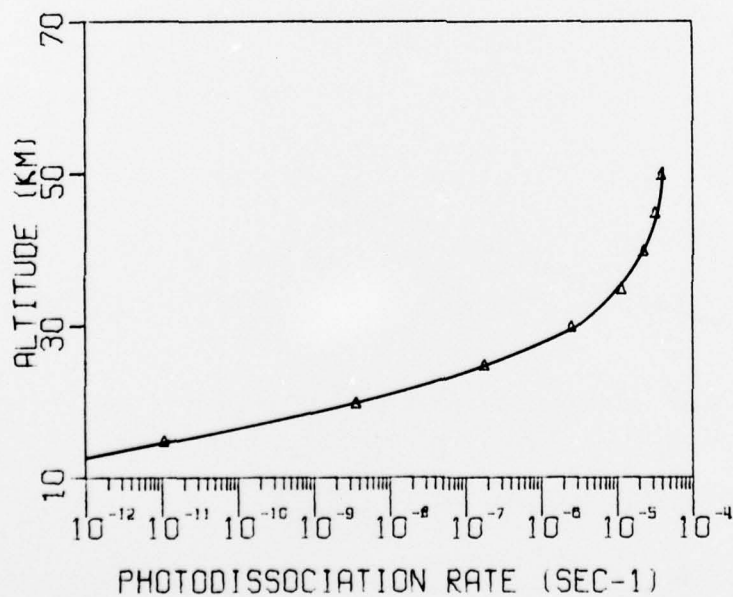
15  $\text{NO}_3 + \text{H}\nu = \text{O} + \text{NO}_2$  [578.0 NM.]  $\phi = 0.10$



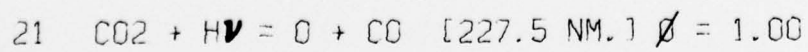
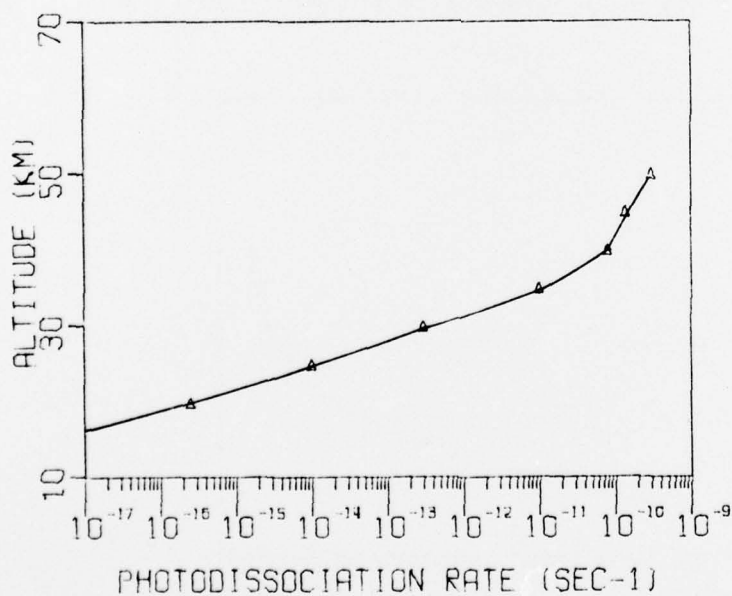
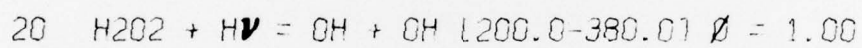
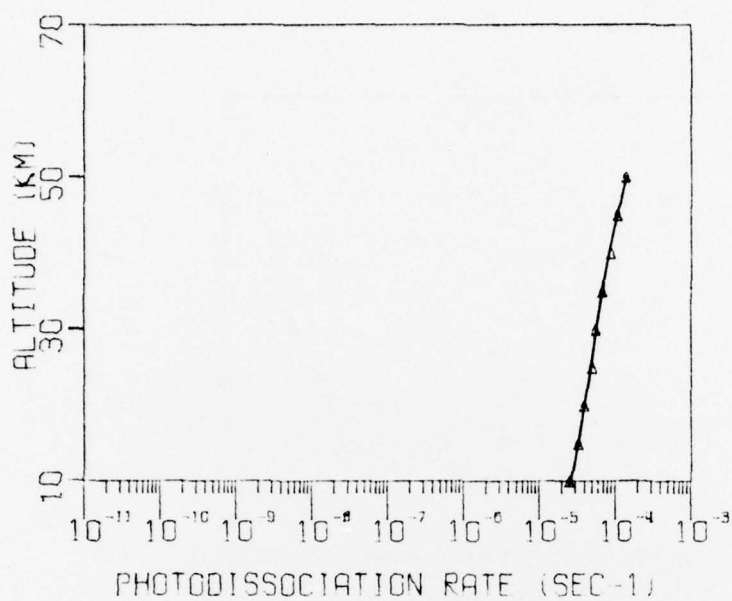
16  $\text{NO}_3 + \text{H}\nu = \text{O}_2 + \text{NO}$  [680.0 NM.]  $\phi = 0.01$

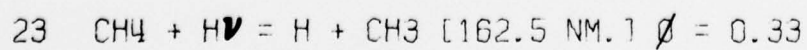
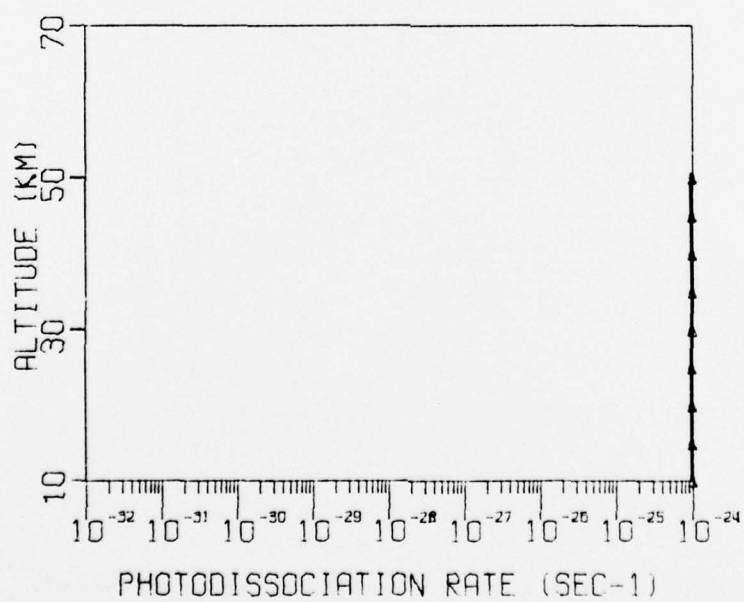
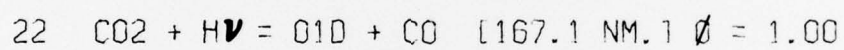
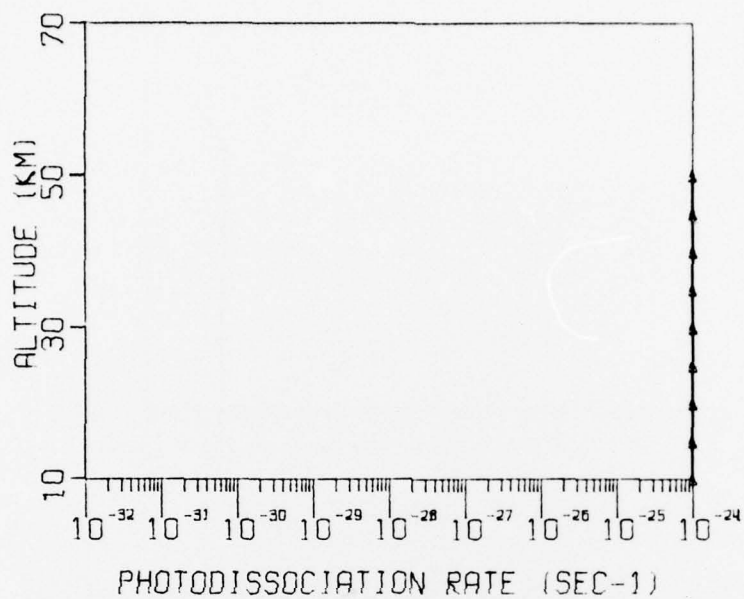


17  $\text{N}_2\text{O}_5 + h\nu = \text{O} + \text{NO}_2 + \text{NO}_2$  [380.0 NM.]  $\phi = 0.50$

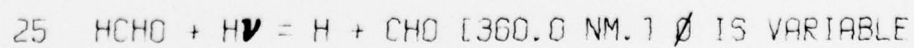
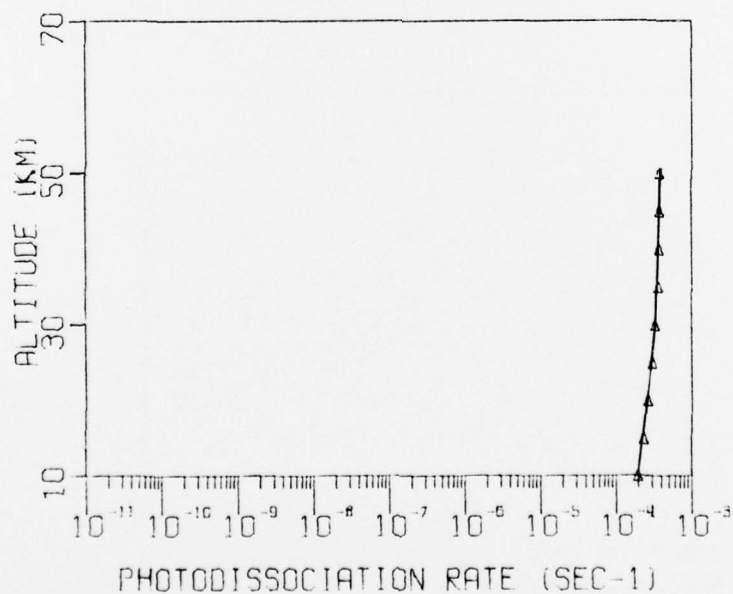
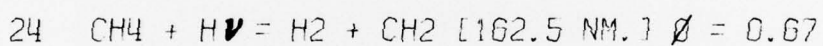
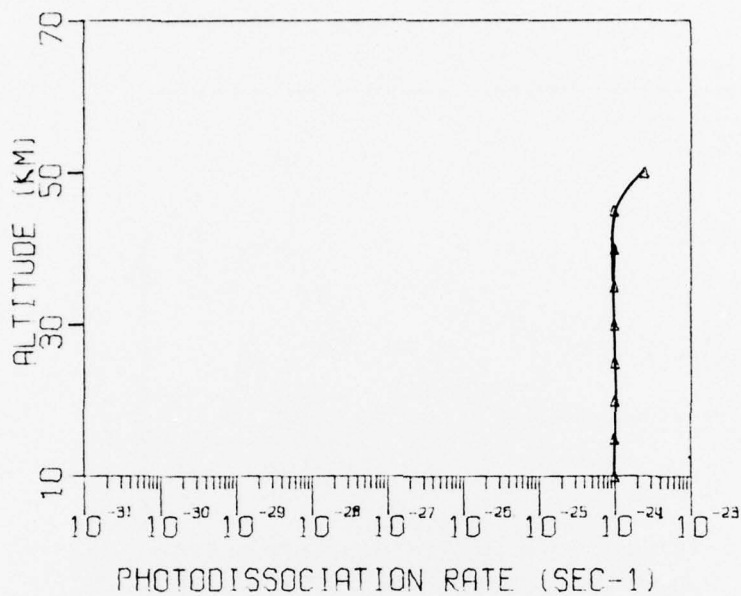


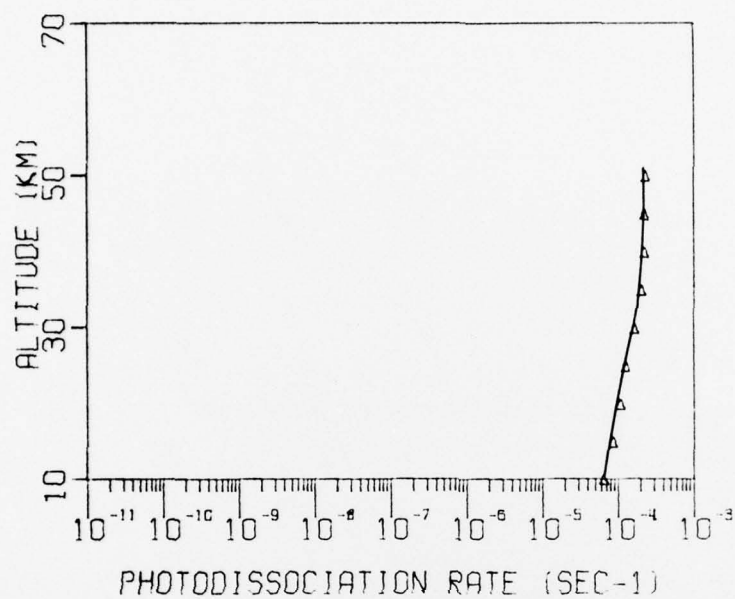
19  $\text{HO}_2 + h\nu = \text{O} + \text{OH}$  [185.0 NM.]  $\phi = 1.00$



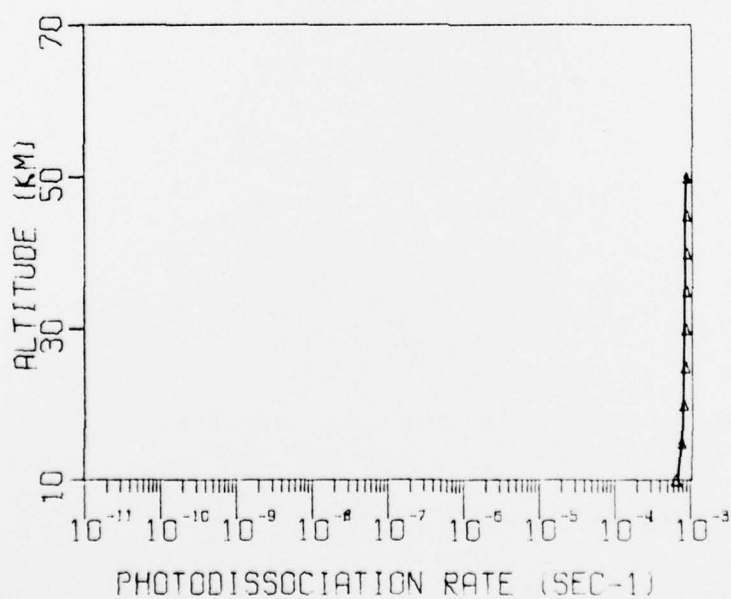




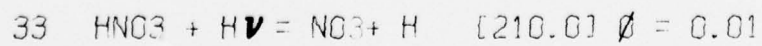
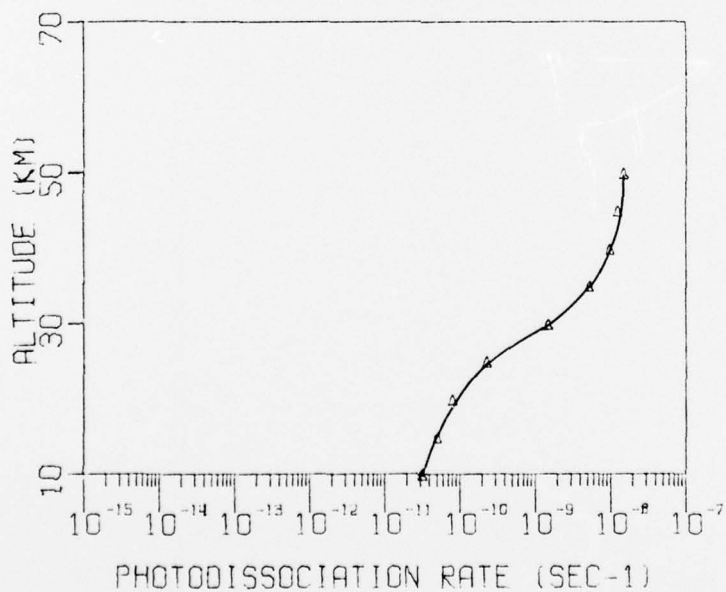
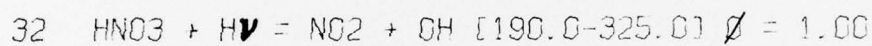
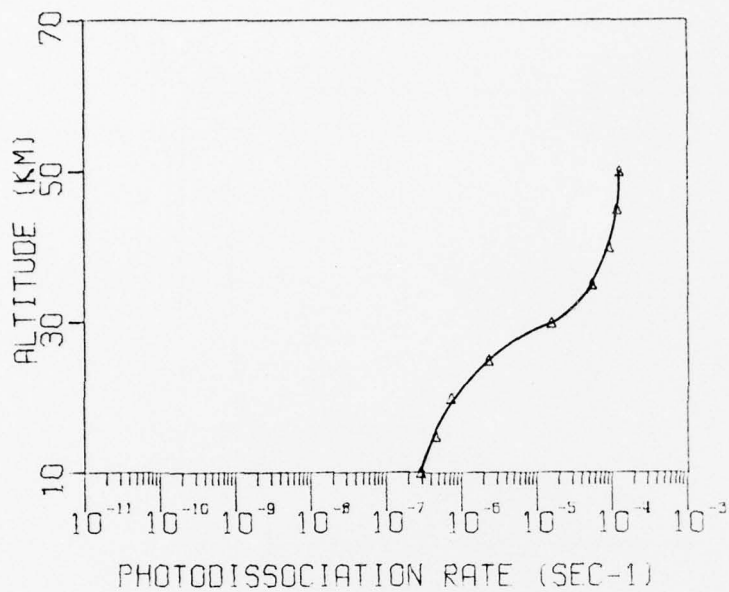




26  $\text{HCHO} + \text{H}\nu = \text{H}_2 + \text{CO}$  [360.0 NM.]  $\phi$  IS VARIABLE



31  $\text{HNO}_2 + \text{H}\nu = \text{NO} + \text{OH}$  [400.0 NM.]  $\phi = 1.00$



# COMPARISON OF PHOTODISSOCIATION RATES

1  $02 + \text{Hv} = 0 + 0$  175.9-242.4 NM.  $\phi = 1.000$

KM.	32 N LATITUDE	65 N LATITUDE
50	.13-08	.11-08
45	.93-09	.80-09
40	.56-09	.46-09
35	.30-09	.10-09
30	.13-09	.20-10
25	.30-10	.29-11
20	.31-11	.56-13
15	.12-12	.14-15
10	.22-14	.49-19

5  $03 + \text{Hv} = 0 + 02$  (440.0)  $\phi = 1.000$

KM.	32 N LATITUDE	65 N LATITUDE
50	.31-03	.31-03
45	.31-03	.31-03
40	.31-03	.30-03
35	.31-03	.30-03
30	.31-03	.29-03
25	.30-03	.29-03
20	.30-03	.29-03
15	.29-03	.29-03
10	.29-03	.27-03

6  $03 + \text{Hv} = 0 + 0210$  310.0-360.0 NM.

KM.	32 N LATITUDE	65 N LATITUDE
50	.10-23	.10-23
45	.10-23	.10-23
40	.10-23	.10-23
35	.10-23	.10-23
30	.10-23	.10-23
25	.10-23	.10-23
20	.10-23	.10-23
15	.10-23	.10-23
10	.10-23	.10-23

7  $03 + \text{Hv} = 010 + 0210$  (310.0 NM.)  $\phi$  IS VARIABLE

KM.	32 N LATITUDE	65 N LATITUDE
50	.46-02	.38-02
45	.33-02	.25-02
40	.16-02	.11-02
35	.72-03	.47-03
30	.33-03	.16-03
25	.11-03	.36-04
20	.43-04	.12-04
15	.22-04	.50-05
10	.16-04	.23-05

8  $0.3 \times H_V = 0.15 \times 0.210$  (199.0 NM.)  $\phi = 0.01$

KM. 32 N LATITUDE 65 N LATITUDE

50	.35-07	.35-07
45	.27-07	.27-07
40	.19-07	.10-07
35	.11-07	.11-08
30	.48-08	.29-09
25	.99-09	.23-10
20	.77-10	.44-12
15	.17-11	.59-15
10	.22-14	.17-20

9  $0.3 \times H_V = 0 \times 0.215$  (266.0 NM.)  $\phi = 0.05$

KM. 32 N LATITUDE 65 N LATITUDE

50	.15-05	.24-06
45	.75-06	.17-06
40	.22-06	.12-05
35	.41-07	.20-07
30	.65-10	.34-10
25	.95-15	.13-15
20	.10-23	.10-23
15	.10-23	.10-23
10	.10-23	.10-23

11  $N02 \times H_V = 0 \times N0$  (>190.0)  $\phi$  IS VARIABLE

KM. 32 N LATITUDE 65 N LATITUDE

50	.14-01	.13-01
45	.14-01	.13-01
40	.13-01	.13-01
35	.13-01	.13-01
30	.13-01	.12-01
25	.13-01	.12-01
20	.12-01	.11-01
15	.12-01	.10-01
10	.11-01	.10-01

12  $N02 \times H_V = 0.10 \times N0$  (<190.0)  $\phi = 0.02-0.05$

KM. 32 N LATITUDE 65 N LATITUDE

50	.35-04	.23-04
45	.30-04	.19-04
40	.21-04	.14-04
35	.12-04	.35-05
30	.49-05	.70-05
25	.97-06	.40-07
20	.92-07	.80-09
15	.44-08	.29-11
10	.17-09	.17-14



13  $N20 + H_V = 010 + N2$  (337.0 NM.)  $\phi = 1.00$

KM.	32 N LATITUDE	65 N LATITUDE
50	.96-03	.94-03
45	.88-03	.57-03
40	.75-08	.51-08
35	.62-03	.33-03
30	.47-03	.27-03
25	.30-08	.15-08
20	.19-03	.74-03
15	.13-08	.39-09
10	.10-03	.90-10

14  $N20 + H_V = N + N0$  (255.0 NM.)  $\phi = 0.01$

KM.	32 N LATITUDE	65 N LATITUDE
50	.11-03	.11-03
45	.10-09	.95-10
40	.81-10	.51-10
35	.57-10	.28-10
30	.29-10	.61-11
25	.75-11	.93-12
20	.76-12	.76-13
15	.24-13	.97-14
10	.19-14	.30-16

15  $N03 + H_V = 0 + N02$  (578.0 NM.)  $\phi = 0.10$

KM.	32 N LATITUDE	65 N LATITUDE
50	.97-03	.97-03
45	.97-03	.97-03
40	.97-03	.97-03
35	.97-03	.97-03
30	.97-03	.96-03
25	.96-03	.96-03
20	.96-03	.96-03
15	.95-03	.95-03
10	.94-03	.94-03

16  $N03 + H_V = 02 + N0$  (680.0 NM.)  $\phi = 0.01$

KM.	32 N LATITUDE	65 N LATITUDE
50	.30-03	.30-03
45	.30-03	.29-03
40	.29-03	.29-03
35	.29-03	.29-03
30	.29-03	.29-03
25	.29-03	.28-03
20	.29-03	.28-03
15	.28-03	.28-03
10	.28-03	.28-03

17  $N205 + HV = 0 + V02 + V02$  (380.0 NM.)  $\delta = 0.50$

KM. 32 N LATITUDE 65 N LATITUDE

50	.23-03	.22-03
45	.20-03	.19-03
40	.15-03	.13-03
35	.10-03	.76-04
30	.60-04	.43-04
25	.38-04	.25-04
20	.27-04	.18-04
15	.23-04	.14-04
10	.21-04	.12-04

19  $V02 + HV = 0 + 04$  (185.0 NM.)  $\delta = 1.00$

KM. 32 N LATITUDE 65 N LATITUDE

50	.52-04	.40-04
45	.44-04	.32-04
40	.31-04	.23-04
35	.18-04	.12-04
30	.82-05	.26-05
25	.19-05	.18-05
20	.20-06	.37-08
15	.86-08	.11-10
10	.24-09	.55-14

20  $H202 + HV = 0H + 0H$  (200.0-380.0 NM.)  $\delta = 1.00$

KM. 32 N LATITUDE 65 N LATITUDE

50	.14-03	.14-03
45	.12-03	.11-03
40	.10-03	.90-04
35	.82-04	.69-04
30	.68-04	.56-04
25	.56-04	.50-04
20	.49-04	.40-04
15	.45-04	.33-04
10	.40-04	.26-04

21  $C02 + HV = 0 + C1$  (227.5 NM.)  $\delta = 1.000$

KM. 32 N LATITUDE 65 N LATITUDE

50	.51-09	.31-09
45	.34-09	.14-09
40	.18-09	.81-10
35	.80-10	.10-10
30	.21-10	.30-12
25	.27-11	.10-13
20	.90-13	.25-15
15	.50-15	.60-19
10	.25-18	.10-23

22  $\text{CO}_2 + \text{H}\nu = \text{O}_1 + \text{CO}$  (167.1 NM.)  $\phi = 1.00$

KM.	32 N LATITUDE	65 N LATITUDE
50	.10-23	.10-23
45	.10-23	.10-23
40	.10-23	.10-23
35	.10-23	.10-23
30	.10-23	.10-23
25	.10-23	.10-23
20	.10-23	.10-23
15	.10-23	.10-23
10	.10-23	.10-23

23  $\text{CH}_4 + \text{H}\nu = \text{H} + \text{CH}_3$  (162.5 NM.)  $\phi = 0.33$

KM.	32 N LATITUDE	65 N LATITUDE
50	.11-16	.10-23
45	.31-23	.10-23
40	.10-23	.10-23
35	.10-23	.10-23
30	.10-23	.10-23
25	.10-23	.10-23
20	.10-23	.10-23
15	.10-23	.10-23
10	.10-23	.10-23

24  $\text{CH}_4 + \text{H}\nu = \text{H}_2 + \text{CH}_2$  (162.5 NM.)  $\phi = 0.57$

KM.	32 N LATITUDE	65 N LATITUDE
50	.85-16	.26-23
45	.94-23	.10-23
40	.10-23	.10-23
35	.10-23	.10-23
30	.10-23	.10-23
25	.10-23	.10-23
20	.10-23	.10-23
15	.10-23	.10-23
10	.10-23	.10-23

25  $\text{HCHO} + \text{H}\nu = \text{H} + \text{CHO}$  (360.0 NM.)  $\phi$  IS VARIABLE

KM.	32 N LATITUDE	65 N LATITUDE
50	.41-03	.39-03
45	.41-03	.39-03
40	.40-03	.38-03
35	.39-03	.37-03
30	.38-03	.34-03
25	.35-03	.31-03
20	.33-03	.27-03
15	.30-03	.24-03
10	.27-03	.20-03

26  $\text{HCHO} + \text{H}\nu = \text{H}_2 + \text{CO}$  (360.0 NM.)  $\phi$  IS VARIABLE

KM. 32 N LATITUDE 65 N LATITUDE

50	.25-03	.24-03
45	.24-03	.23-03
40	.24-03	.23-03
35	.22-03	.21-03
30	.20-03	.17-03
25	.17-03	.13-03
20	.14-03	.11-03
15	.12-03	.87-04
10	.11-03	.66-04

31  $\text{HNO}_2 + \text{H}\nu = \text{NO} + \text{OH}$  (400.0 NM.)  $\phi = 1.00$

KM. 32 N LATITUDE 65 N LATITUDE

50	.93-03	.88-03
45	.93-03	.88-03
40	.93-03	.87-03
35	.92-03	.87-03
30	.91-03	.86-03
25	.89-03	.83-03
20	.88-03	.83-03
15	.86-03	.74-03
10	.79-03	.63-03

32  $\text{HNO}_3 + \text{H}\nu = \text{NO}_2 + \text{OH}$  (170.0-325.0 NM.)  $\phi = 1.0$

KM. 32 N LATITUDE 65 N LATITUDE

50	.13-03	.13-03
45	.12-03	.12-03
40	.95-04	.73-04
35	.68-04	.55-04
30	.37-04	.16-04
25	.11-04	.23-05
20	.23-05	.74-05
15	.10-05	.46-06
10	.79-05	.29-05

33  $\text{HNO}_3 + \text{H}\nu = \text{NO}_3 + \text{H}$  (210.0)  $\phi = 0.01$

KM. 32 N LATITUDE 65 N LATITUDE

50	.15-07	.15-07
45	.13-07	.13-07
40	.11-07	.13-07
35	.76-08	.54-08
30	.41-08	.15-08
25	.12-08	.23-09
20	.25-09	.42-10
15	.11-09	.51-10
10	.88-10	.32-10